

The use of slow waves to design simple sound absorbing materials

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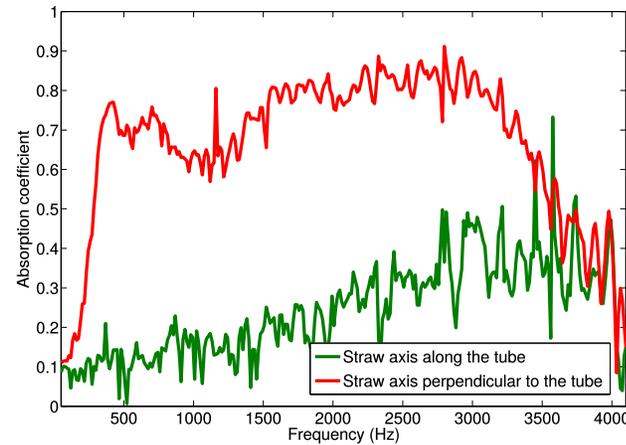
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in collaboration with

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Motivation

1. Straw as acoustic absorbers



2. Evidence of slow sound in induced transparency band (narrow freq. band)

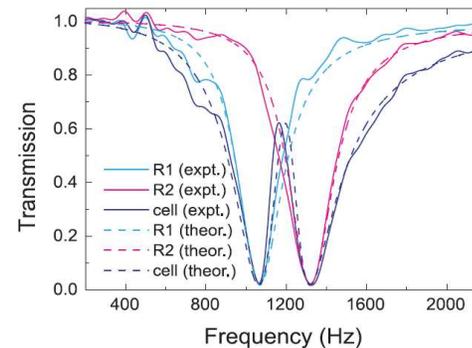
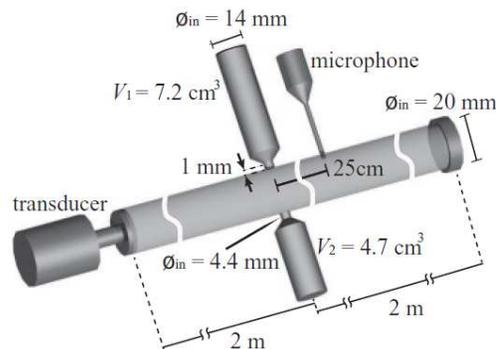
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Acoustic transparency and slow sound using detuned acoustic resonators

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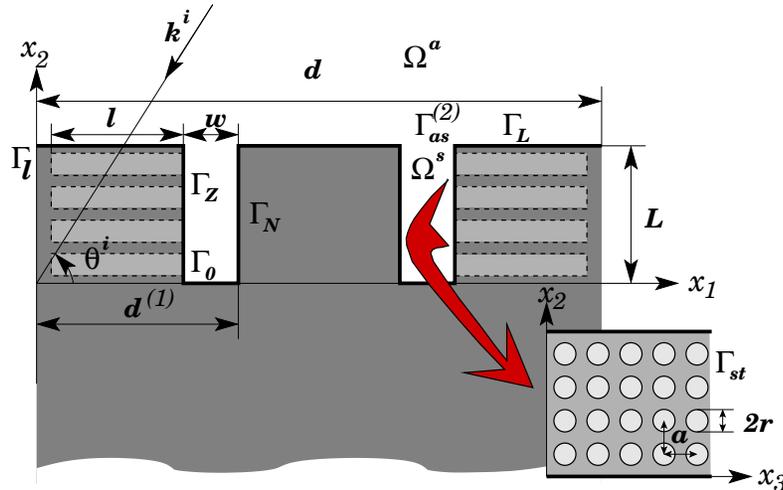
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⇒ Use slow sound to absorb sound at low frequencies

Description of the configuration

Propagation in the tube and in the narrow irregularities (Stinson, J. Acoust. Soc. Am., 1991)



Look for $p^g(\mathbf{x}, \omega)$, $\forall \mathbf{x} \in \Omega^g$, $s = a, s, t$,

$$\left\{ \begin{array}{l} (\nabla + (k^g)^2)p^g(\mathbf{x}) = 0, \quad \forall \mathbf{x} \in \Omega^s, \quad g = a, s, t \\ k^a = \omega/c^a, \quad k^g = \omega/c^g(\omega), \quad g = s, t \\ + \\ p^a(\mathbf{x}) - p^i(\mathbf{x}) \sim \text{outgoing waves; } |\mathbf{x}| \rightarrow \infty, \quad x_2 \geq L, \end{array} \right.$$

wherein $p^i(\mathbf{x}) = A^i e^{i\mathbf{k}_1^i x_1 - i\mathbf{k}_2^{a_i}(x_2 - L)}$

$$\text{Boundary conditions: } \left\{ \begin{array}{l} [p(\mathbf{x})] = 0, \quad \forall \mathbf{x} \in \Gamma_{as}, \\ [(\rho(\mathbf{x}))^{-1} \partial_n p(\mathbf{x})] = 0, \quad \forall \mathbf{x} \in \Gamma_{as}, \Gamma_N, \Gamma_L, \Gamma_0 \\ \mathbf{V}^s \cdot \mathbf{n} / p^s(\mathbf{x}) = Z, \quad \forall \mathbf{x} \in \Gamma_Z, \end{array} \right.$$

The field is quasi-periodic (*Floquet-Bloch condition*):

$$p(x_1 + qd_1, x_2) = p(x_1, x_2) e^{ik_1^i qd}, \quad \forall \mathbf{x} \in \mathbb{R}^2 \text{ and } \forall (q) \in \mathbb{Z}.$$

⇒ It is sufficient to determine the field in the unit cell \mathcal{C} .

Solution of the problem

Domain decomposition method, field expressions: Bloch waves

$$p^a(\mathbf{x}) = \sum_{q \in \mathbb{Z}} \left[A^i e^{-ik_{2q}^a(x_2-L)} \delta_q + R_q e^{ik_{2q}^a(x_2-L)} \right] e^{ik_{1q}^a x_1}, \text{ with } k_{1q}^a = k_1^i + \frac{2q\pi}{d}.$$

Modal representation in Ω^s

$$p^{s(n)} = \sum_{m \in \mathbb{N}} A_n \cos \left(k_{1m}^s \left(x_1 - d^{(n)} \right) \right) \cos \left(k_{2m}^s x_2 \right) \forall \mathbf{x} \in \Omega^{(n)},$$

wherein modes are bi-orthogonal (Lawrie, Q.J.I.Mech.Apl.Math., 1999) and satisfy

$$k_{1m}^s \tan(k_{1m}^s w) = \frac{-i\omega\rho^s}{Z} \text{ with } Z = \frac{iZ^t \cotan(k^t l)}{\phi^t}, \text{ and surface porosity } \phi^t = \frac{\pi r^2}{a^2},$$

Application of the B.C. on $\Gamma_{as}^{(n)}$ lead to

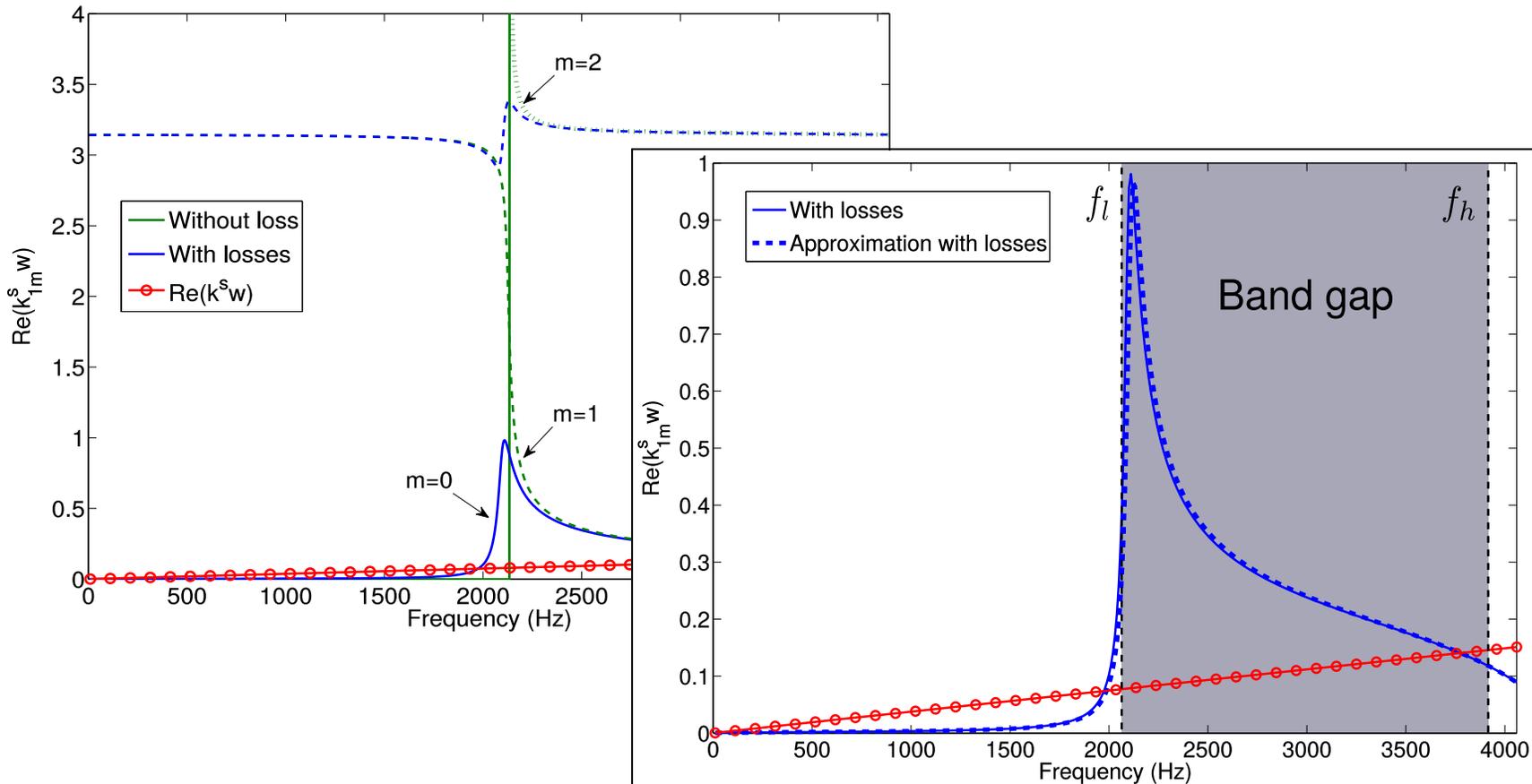
$$R_q - \frac{i\rho^a}{k_{2q}^a} \sum_{Q \in \mathbb{Z}} R_Q \sum_{n \in \mathcal{N}} \sum_{m \in \mathbb{Z}} \frac{k_{2m}^s \phi^{s(n)}}{\rho^s N_m} \tan(k_{2m}^s L) I_{mq}^{l/r(n)-} I_{mQ}^{l/r(n)+} =$$

$$A^i \delta_q + A^i \sum_{n \in \mathcal{N}} \sum_{m \in \mathbb{Z}} \frac{i\rho^a k_{2m}^s \phi^{s(n)}}{k_{2q}^a \rho^s N_m} \tan(k_{2m}^s L) I_{mq}^{l/r(n)-} I_{m0}^{l/r(n)+},$$

wherein $\phi^{s(n)} = w/d$ is the surface porosity of one slit, such that $\bigcup_{n \in \mathcal{N}} \phi^{s(n)} = \phi^s$

Dispersion relation: $k_{1m}^s \tan(k_{1m}^s w) = -i\omega\rho^s/Z$

$r = 2.5$ mm, $a = 7$ mm ($\phi^t \approx 0.4$), $l = 40$ mm, $w = 2$ mm

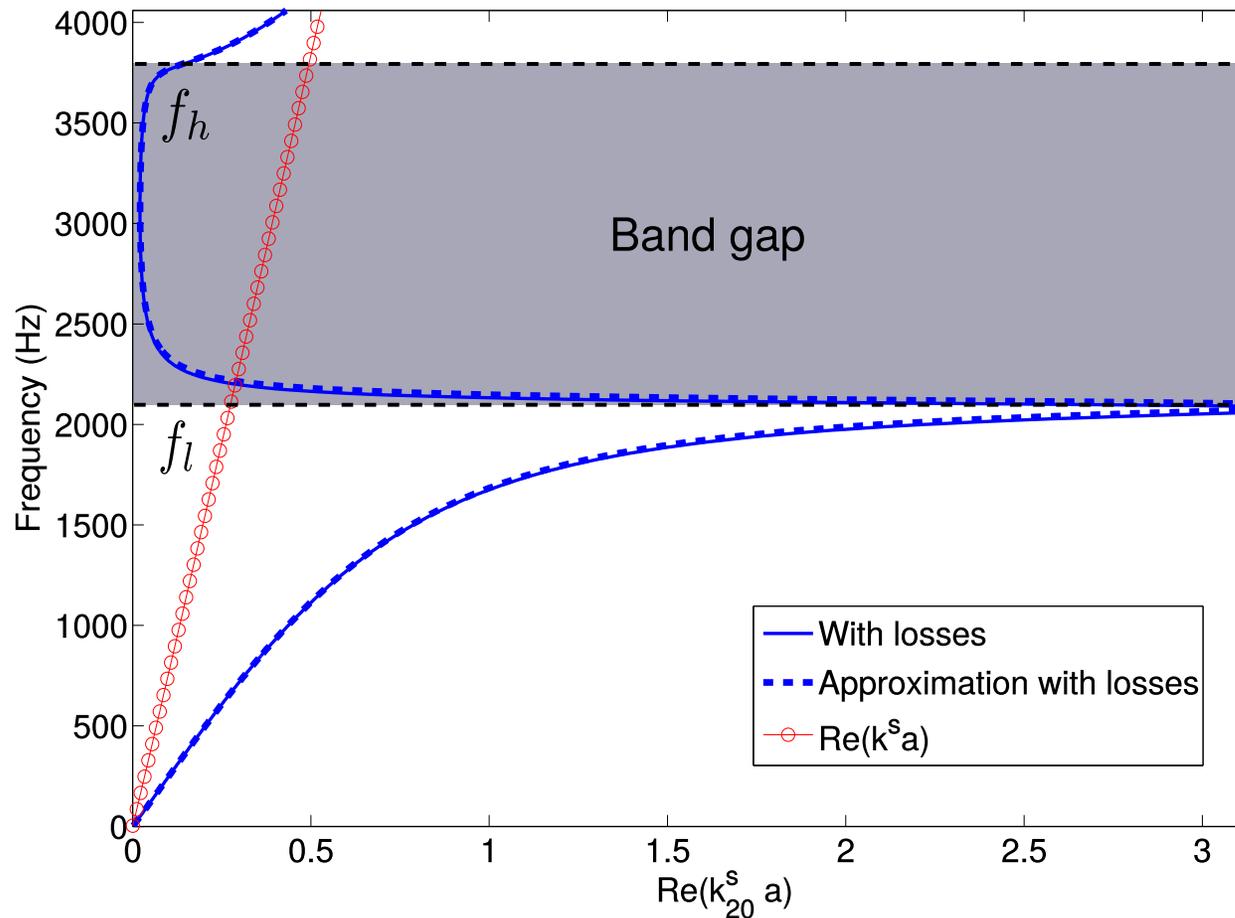


k_{10}^s correctly approximated by $\tilde{k}_{10}^s = 1/w \sqrt{-i\omega\rho^s w/Z}$

Lower and higher bounds of the BG: $f_l \approx c^t/4l$ and $f_h = 1/(2(l/c^t + wZ^t/c^s Z^s \phi^t))$

A more common representation

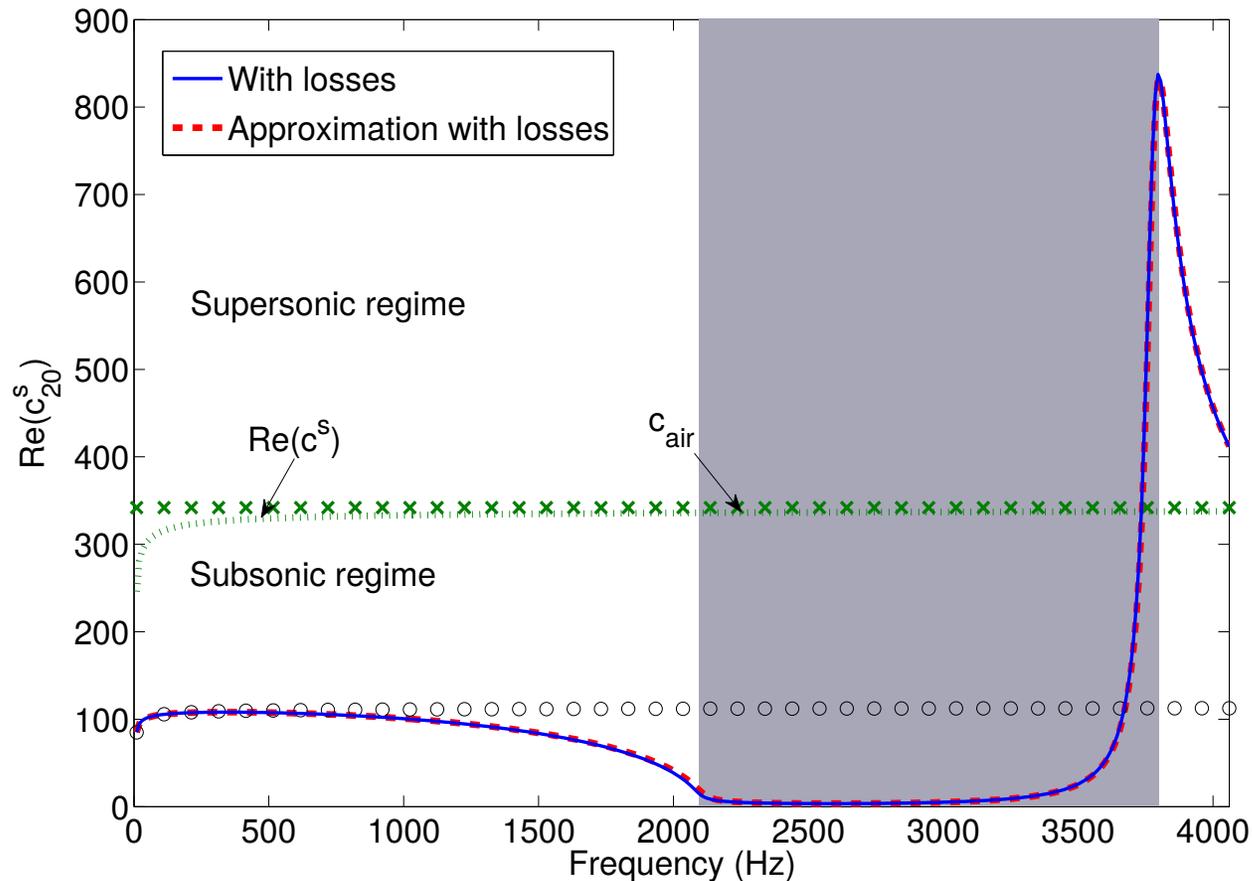
We look at $\text{Re}(k_{20}^s a)$, normalized wavenumber of the wave travelling in the slit



Below f_l , the slope of $\text{Re}(k_{20}^s a)$ is always smaller than the one of $\text{Re}(k^s a)$

Evidence of slow sound

We look at $\text{Re}(c_{20}^s) = w/k_{20}^s = w/\sqrt{(k^s)^2 - (k_{10}^s)^2}$, speed of sound travelling in the slit



$$\lim_{\omega \rightarrow 0} c_{20}^s(\omega) \approx c^s / \sqrt{1 + \frac{\phi^t l Z^s c^s}{w Z^t c^t}}; \text{ without loss } \lim_{\omega \rightarrow 0} c_2^s \approx c^a / \sqrt{1 + \frac{\phi^t l}{w}}$$

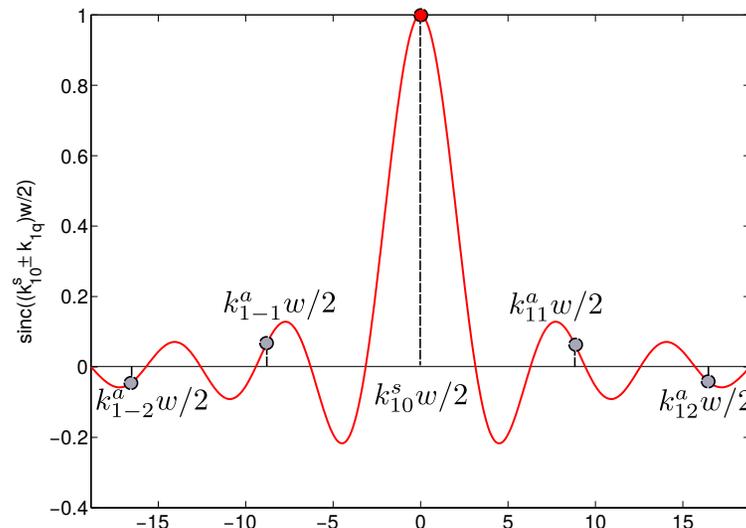
Sound speed & attenuation can be tuned by the ratio $\frac{\phi^t l}{w}$ and $\text{Im}(k_{20}^s(\omega)) > \text{Im}(k^s)$

Assumption to derive of the effective parameters

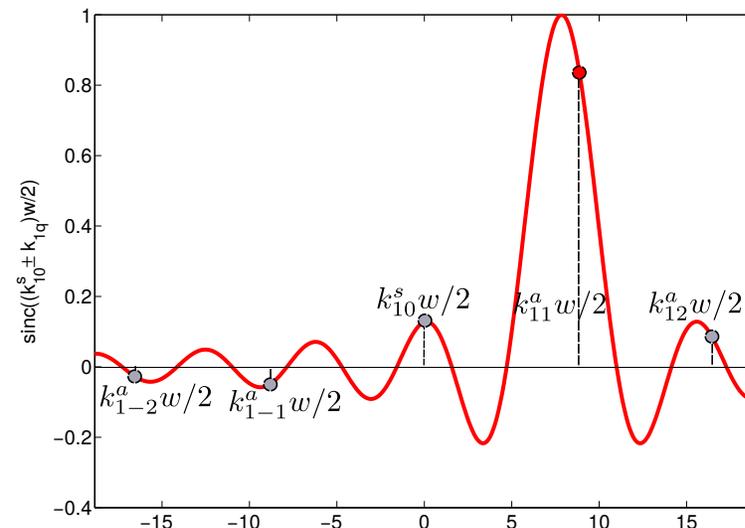
We assume $k_{10}^s w \ll 1$ so $N_0 \approx 1$.

$I_{0q}^{l/r(n)\pm}$ depends on $\text{sinc}\left((k_{10}^s \pm k_{1q}^a)w/2\right)$; at normal incidence $k_1^i = 0$, we have

Only 0-th order Bloch mode contribute



1-st order Bloch mode also contribute



k_{10}^s being dispersive close to f_l , higher order Bloch modes contribute to the field

When $\left| (k_{10}^s \pm k_{11}^a) \frac{w}{2} \right| \gg 1$, $\text{sinc}\left((k_{10}^s \pm k_{11}^a) \frac{w}{2}\right) \approx 1$ and $I_{00}^{l/r(n)\pm} \approx 1$, we have

$$R_0 = A^i \frac{i\omega\rho^s \cot(k_{20}^s L) / \phi^s k_{20}^s - Z_0 / \sin\theta^i}{i\omega\rho^s \cot(k_{20}^s L) / \phi^s k_{20}^s + Z_0 / \sin\theta^i}.$$

The effective parameters

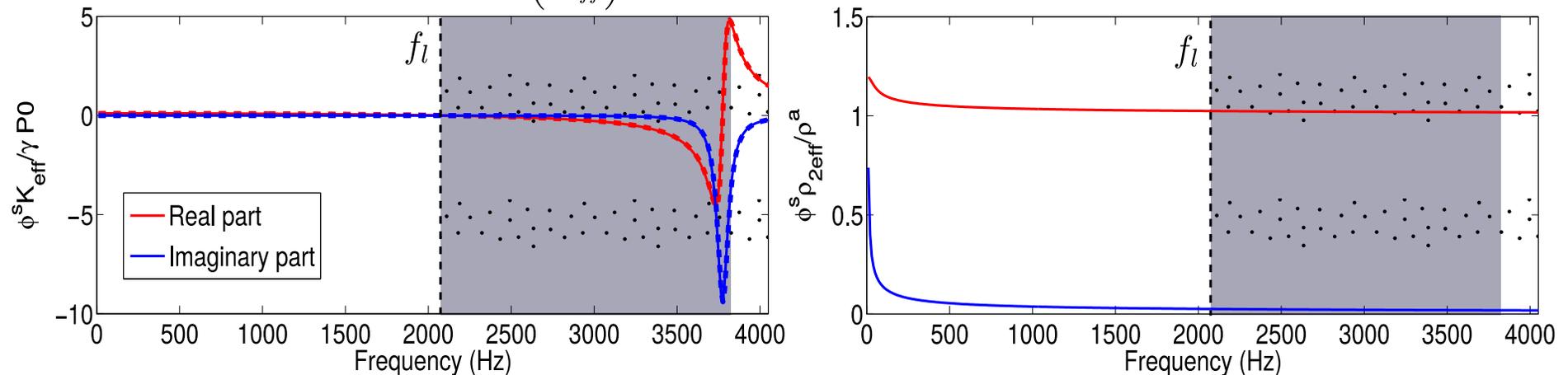
From which we can identify an effective anisotrop medium (locally reacting material)

$$\bar{\rho}_{eff} = \begin{pmatrix} 0 & 0 \\ 0 & \frac{\rho^s}{\phi^s} \end{pmatrix},$$

$$K_{eff}^s = \frac{K^s}{\phi^s (1 + Z^s \phi^t \tan(k^t l) / Z^t k^s h)}.$$

$r = 2.5 \text{ mm}$, $a = 7 \text{ mm}$ ($\phi^t \approx 0.4$), $N = 1$, $l = 40 \text{ mm}$, $w = 2 \text{ mm}$, $d = 42 \text{ mm}$

$\text{Re}(K_{eff}^s) < 0$ (Fang et al., Nature Mat., 2006)

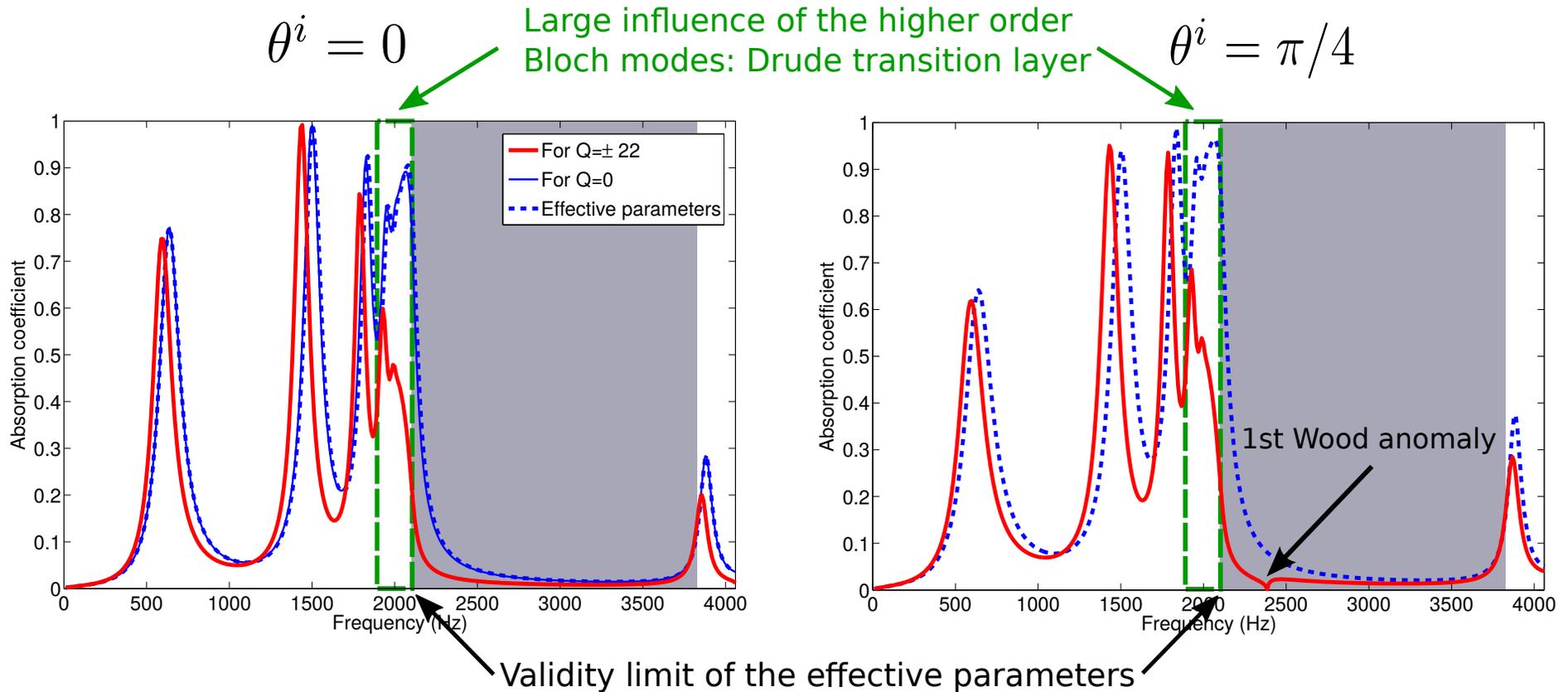


In the slit $\rho_{eff}^s = \rho_{2eff} \phi^s = \rho^s$ and $K_{eff}^s = K_{eff} \phi^s$

Only K_{eff}^s is modified! Slow sound cannot be due to α_∞ ; only thermal effect

The absorption curves

$L = 42$ mm, $N = 2$, $d = 84$ mm, $d^{(1)} = 42$ mm (Γ_Z , left) and $d^{(2)} = 42$ mm (Γ_Z , right)

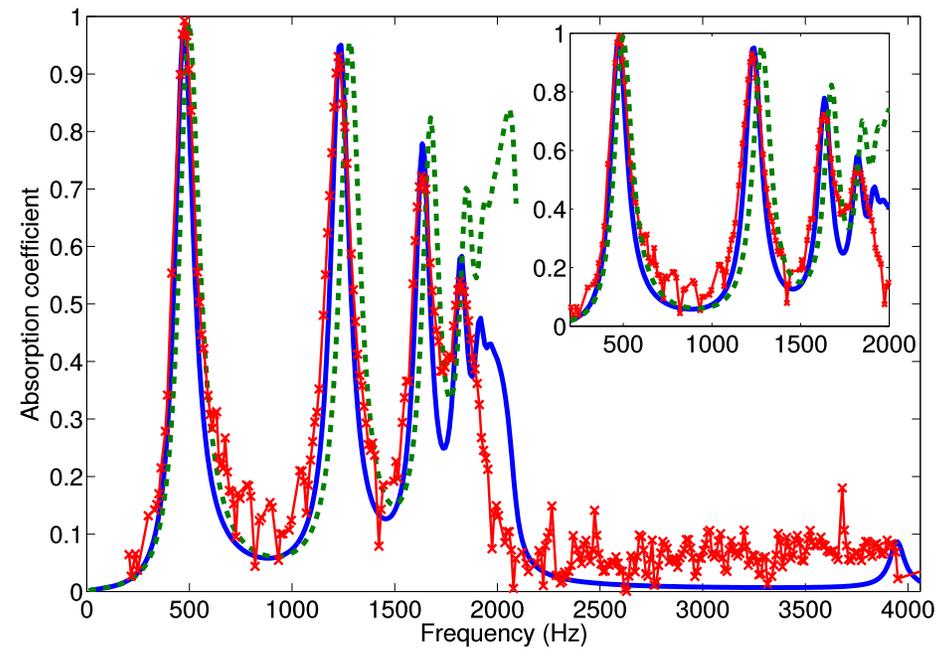
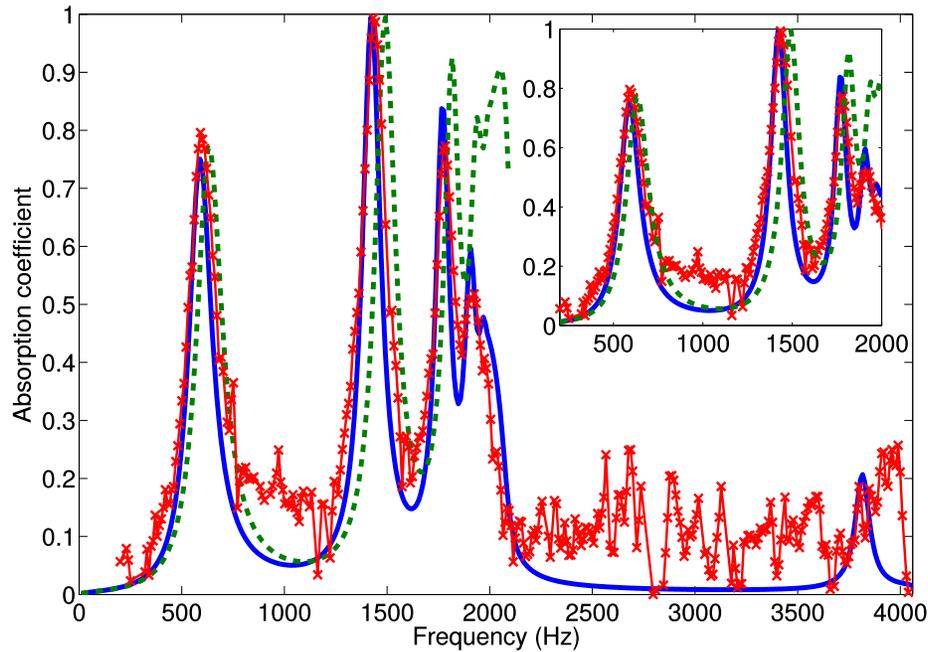
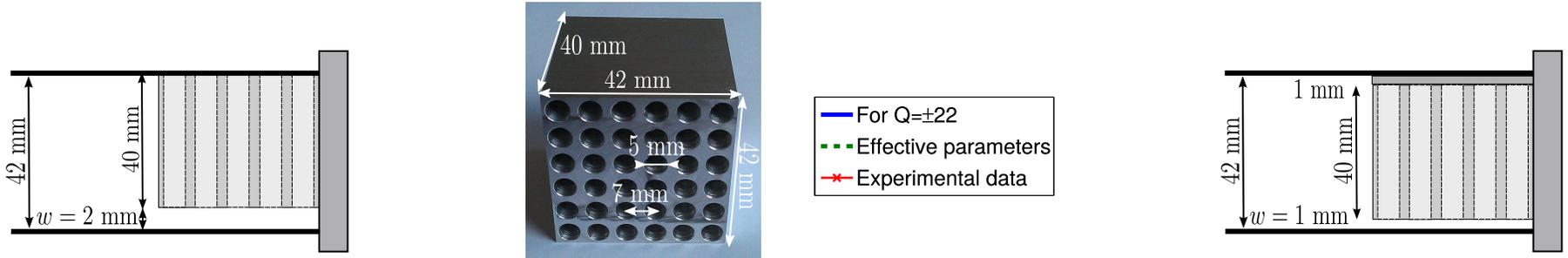


Effective parameters accurate below f_l : evidence of the Drude transition layers

Large absorption peak at 590 Hz: $\lambda^a \approx 14 \times L$

Experimental validation

Square impedance tube to create the periodic pattern



Linearity has been checked & validated (two different amplitudes)

Conclusion & perspectives

- Slow sound enable to lower the quarter-wavelength resonance frequency
 - ⇒ Design a sound absorbing metamaterial
- Derivation of the effective properties
 - ⇒ Slow sound induced by a modification of K_{eff} ; it is not due to α_∞
 - ⇒ Evidence of the Drude layer and validity limit
- Current work
 - ⇒ 3D rectangular pores with various types of resonators plugged on it
 - ⇒ Broaden the absorption frequency band by detuning resonators
- Perspectives
 - ⇒ Study wave propagation in waveguides with graded resonances
 - ⇒ More complex model for the straw (accounting for the irregularities?)

J.-P. Groby, W. Huand, A. Lardeau, and Y. Aurégan, *The use of slow sound to design simple sound absorbing materials*, submitted to Journal of Applied Physics in Sept. 2014.

Thank you for your attention



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